

Differential Semblance Migration Velocity Analysis via Reverse Time Migration: Gradient Computation

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- 1 Introduction
- 2 RTM Formula and DSMVA Objective Function
- 3 Gradient Computation
- 4 Summary
- 5 Future Work
- 6 Appendix: Gradient Computation

- Differential Semblance Velocity Analysis
 - Smoothness
 - Convexity
- Reverse Time Migration
 - Dip limitation
- DSMVA-RTM

Acoustic wave equation with constant density

$$\left(\frac{1}{c^2(\mathbf{x})} \frac{\partial^2}{\partial t^2} - \nabla^2 \right) p(\mathbf{x}, t; \mathbf{x}_s) = f(t) \delta(\mathbf{x} - \mathbf{x}_s)$$

\mathbf{x} = position vector

\mathbf{x}_s = position of the point source

$c(\mathbf{x})$ = velocity

$p(\mathbf{x}, t; \mathbf{x}_s)$ = pressure

Source time function $f(t) = \delta(t)$

Two-way wave equation operator $\mathbf{L} := \frac{1}{c^2(\mathbf{x})} \frac{\partial^2}{\partial t^2} - \nabla^2$

Source Wavefields (forward in time):

$$\begin{aligned} \mathbf{L}S(\mathbf{x}, t; \mathbf{x}_s) &= \delta(t)\delta(\mathbf{x} - \mathbf{x}_s) \\ S &\equiv 0 \text{ for } t < 0 \end{aligned}$$

Receiver Wavefields (backwards in time):

$$\begin{aligned} \mathbf{L}R(\mathbf{x}, t; \mathbf{x}_s) &= \int d(\mathbf{x}_r, t; \mathbf{x}_s)\delta(\mathbf{x} - \mathbf{x}_r) d\mathbf{x}_r \\ R &\equiv 0 \text{ for } t > t_{max} \end{aligned}$$

Write

$$c(\mathbf{x}) = v(\mathbf{x}) + \delta v(\mathbf{x}).$$

Forward Born Modeling:

$$F[v]\delta v = \delta S|_{surface}$$

Adjoint of Forward Modeling:

$$F^* d = l$$

Migration formula:

$$I(\mathbf{x}, h) = \int S(\mathbf{x} + h, t; \mathbf{x}_s) R(\mathbf{x} - h, t; \mathbf{x}_s) d\mathbf{x}_s dt$$

DSMVA-RTM objective function:

$$J[v] = \frac{1}{2} \|PI\|^2$$

Gradient Computation

For $u = P^*PI$, DI^*u gives the gradient.

Introducing g_r solving

$$\begin{aligned}\mathbf{L}g_r(\mathbf{x}, t; \mathbf{x}_s) &= \int R(\mathbf{x} - 2h, t; \mathbf{x}_s)u(t - h, h) dh \\ g_r &\equiv 0 \text{ for } t > t_{max}, BC\end{aligned}$$

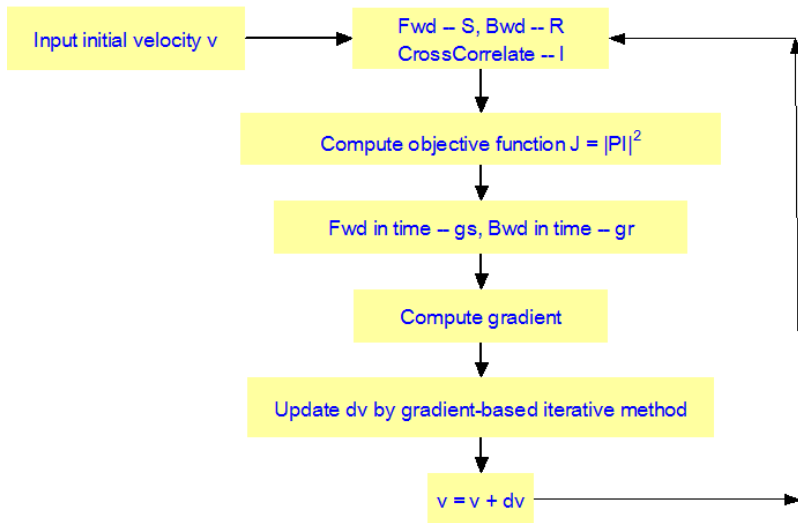
Introducing g_s solving

$$\begin{aligned}\mathbf{L}g_s(\mathbf{x}, t; \mathbf{x}_s) &= \int S(\mathbf{x} + 2h, t; \mathbf{x}_s)u(t + h, h) dh \\ g_s &\equiv 0 \text{ for } t < 0, BC\end{aligned}$$

The gradient of DSMVA-RTM is

$$\nabla_v J = \int \frac{2}{v^3} \left(\frac{\partial^2 S}{\partial t^2} g_r + \frac{\partial^2 R}{\partial t^2} g_s \right) d\mathbf{x}_s dt$$

Inversion procedure



Comparison between one-way and two-way WEMVA

One-way wave equation migration:

- Pros: low computational cost
- Cons: dip limitation

Two-way wave equation migration:

- Pros: no dip limitation
- Cons: high computational cost
- Cons: amplitude correction required

- Amplitude Correction (see Rami's work)
- Modification of existing RTM code based on SEAMX, TSOpt to compute objective function and to verify its convexity
- Future modification to create gradient
- Comparison with DS based on downward continuous extrapolation

Perturbation of objective function:

$$\delta J = \frac{1}{2} \langle \delta(PI), PI \rangle + \frac{1}{2} \langle PI, \delta(PI) \rangle$$
$$\implies \delta J = \langle \delta c, \text{Re}((DI)^* P^* PI) \rangle$$

Gradient of objective function:

$$\nabla_c J = \text{Re}\{(DI)^*(P^* PI)\}$$

For arbitrary $u(x, h)$, we have

$$\langle \delta I, u \rangle = \langle DI \delta c, u \rangle = \langle \delta c, DI^* u \rangle$$

When $u = P^* PI$, $DI^* u$ gives the gradient.

$$\begin{aligned}
\langle \delta I, u \rangle &= \int \bar{\delta I} u(x, h) dx dh \\
&= \int \delta S(x + h, x_s, t) \bar{R}(x - h, x_s, t) u(x, h) dx dx_s dt dh \\
&\quad + \int S(x + h, x_s, t) \bar{\delta R}(x - h, x_s, t) u(x, h) dx dx_s dt dh \\
&= \int \delta S(x, x_s, t) \left\{ \int \bar{R}(x - 2h, x_s, t) u(x - h, h) dh \right\} dx dx_s dt \\
&\quad + \int \bar{\delta R}(x, x_s, t) \left\{ \int S(x + 2h, x_s, t) u(x + h, h) dh \right\} dx dx_s dt
\end{aligned}$$

Introducing g_r solving

$$\mathbf{L}g_r(\mathbf{x}, t; \mathbf{x}_s) = \int R(\mathbf{x} - 2h, t; \mathbf{x}_s)u(t - h, h) dh$$

$$\int_{\Sigma} \nabla S g_r - S \nabla g_r = 0$$

$$\frac{\partial S}{\partial t} g_r - S \frac{\partial g_r}{\partial t}(\mathbf{x}, 0; \mathbf{x}_s) = 0$$

$$\frac{\partial S}{\partial t} g_r - S \frac{\partial g_r}{\partial t}(\mathbf{x}, t_{max}; \mathbf{x}_s) = 0$$

Introducing g_s solving

$$\mathbf{L}g_s(\mathbf{x}, t; \mathbf{x}_s) = \int S(\mathbf{x} + 2h, t; \mathbf{x}_s)u(t + h, h) dh$$

$$\int_{\Sigma} \nabla R g_s - R \nabla g_s = 0$$

$$\frac{\partial R}{\partial t} g_s - R \frac{\partial g_s}{\partial t}(\mathbf{x}, 0; \mathbf{x}_s) = 0$$

$$\frac{\partial R}{\partial t} g_s - R \frac{\partial g_s}{\partial t}(\mathbf{x}, t_{max}; \mathbf{x}_s) = 0$$

Then,

$$\begin{aligned}\langle \delta I, u \rangle &= \int (\delta S \mathbf{L} g_r + \delta R \mathbf{L} g_s) dx dx_s dt \\ &= \int ((\mathbf{L} \delta S) g_r + (\mathbf{L} \delta R) g_s) dx dx_s dt \\ &= \int \frac{2\delta c}{c^3} \frac{\partial^2 S}{\partial t^2} g_r + \frac{2\delta c}{c^3} \frac{\partial^2 R}{\partial t^2} g_s dx dx_s dt\end{aligned}$$

Thus

$$\nabla_c J = \int \frac{2}{c^3} \left(\frac{\partial^2 S}{\partial t^2} g_r + \frac{\partial^2 R}{\partial t^2} g_s \right) dx_s dt$$